

New Features and Enhancements in StressCheck 10.5



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New Features and Enhancements in SC 10.5



- New Force/moment method
- New TLAP Cross section option
- TLAP Bearing and Bearing loads correction
- New Any Body option for Assignment
- Plastic Strain extractions
- Log Improvements for Incremental Solutions
- Name sorting for ITP solutions
- Face/Face Surface element blank
- Curves resolution can now be controlled
- File Build number is now recorded in the Project Log
- Long solution names are now wrapped on the Plot legend
- <u>Automatic And Manual Selection Of Graphic Drivers</u>



New Force/Moment Option

- STRESSCHECK
- Force/Moment: The directional components of the force and moment vectors are converted into a statically equivalent linear traction distribution, applied over the selected element faces.



 M_{y_c}

• F_{yc}

С

 x_{c}

dA

 F_{z_c}

Load assignment

 M_{x_c}

 M_{z_c}

 The linear traction distribution will be computed along the orthogonal principal axis through the centroid of the section, based on the following definitions:

$$F_{x_c} = \iint T_{x_c} \, dA \qquad M_{x_c} = \iint T_{z_c} \, y_c \, dA$$

$$F_{y_c} = \iint T_{y_c} \, dA \qquad M_{y_c} = - \iint T_{z_c} \, x_c \, dA$$

$$F_{z_c} = \iint T_{z_c} dA \qquad M_{z_c} = \iint T_{y_c} x_c dA - \iint T_{x_c} y_c dA$$

The shear components of the linear traction distributions generated by the Force/Moment option do not satisfy the stress free boundary conditions for general cross sectional shapes. Extractions near the area of load application are discouraged.

STF

$$T_{x_c} = \frac{F_{x_c}}{A} - \frac{1}{2} \frac{M_{z_c}}{I_{x_c}} y_c \qquad T_{y_c} = \frac{F_{y_c}}{A} + \frac{1}{2} \frac{M_{z_c}}{I_{y_c}} x_c \qquad T_{z_c} = \frac{F_{z_c}}{A} - \frac{M_{y_c}}{I_{y_c}} x_c + \frac{M_{x_c}}{I_{x_c}} y_c$$

GUI Changes for Force/Moment. StressCheck Input StressCheck Input

Force/Moment Option



 The selection needs to satisfy a coplanar condition. If the this condition is not satisfied an error issued and the record creation is prevented:

ERROR

Load error found in surfaces/elements = # and #. Force/Moment load applied to faces that are not coplanar. Tolerance may be controlled with parameter <u>COPLANAR_TOL</u> (default=0.0001, use a larger value to loosen the tolerance).

STRESSCHECK

While continuity is not a requirement (multiple selections are allowed) this assignment requires checking a flatness tolerance for the selection (similar as it is done for symmetry or anti-symmetry). If the flatness check does not pass an error is issued and the record is not created:

ERROR

Load error found in surface/element = #. Force/Moment load applied to a surface/face which is not flat. Tolerance may be controlled with parameter _SURFACE_TOL (default=0.001 deg.).

Number of points checked on each surface/face controlled with parameter _SURFACE_MIDPT (default=2). Select surface/face set "_FAIL_LOAD" to see problem surfaces/faces.

- Only Direction: XYZ is allowed, if a non-Cartesian system is selected an error is issued and the record is not created.
- Only numeric or parametric input are to be allowed, with exception of formulae used as parametric expression (i.e., with the pipe "|" symbol preceding the formula name).
- Shown for "Face Surface" but also available for "Face" Object

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New Method









Selections are flat but not coplanar, an error is issued when pressing "Accept"

ERROR

Load error found in elements = # and #, case = LOAD_ID. Force/Moment load applied to faces that are not coplanar. Tolerance may be controlled with parameter _COPLANAR_TOL (default=0.0001, use a larger value to loosen the tolerance).

ERROR

Load error found in surfaces # and #. Force/Moment load applied to surfaces that are not coplanar. Tolerance may be controlled with parameter _COPLANAR_TOL(default = 0.0001, use a larger value to loosen the tolerance). Cross Section







ERROR

Load error found in surface = #. Force/Moment load applied to a surface which is not flat. Tolerance may be controlled with parameter _SURFACE_TOL (default = 0.001 deg.). Number of points checked on each surface controlled with parameter _SURFACE_MIDPT(default = 2).Select surface set "_FAIL_LOAD" to see problem surfaces.

ERROR

Load error found in element = #. Force/Moment load applied to a surface which is not flat. Tolerance may be controlled with parameter _SURFACE_TOL (default=0.001 deg.). Number of points checked on each face controlled with parameter _SURFACE_MIDPT (default=2). Select surface set "_FAIL_LOAD" to see problem surfaces.

Cross Section







New TLAP Cross Section Option



 TLAP-Traction (Cross Section): The TLAP force and moment components are converted into a statically equivalent linear traction distribution, applied over the selected element faces.



 M_{y_c}

 F_{y_c}

С

 x_{c}

dA

 F_{z_c}

 M_{z_c}

Load assignment

The linear traction distribution will be computed along the orthogonal principal through the centroid of the section, based on the following definitions:

$$F_{x_c} = \iint T_{x_c} \, dA \qquad M_{x_c} = \iint T_{z_c} \, y_c \, dA$$
$$M_{x_c} \qquad F_{y_c} = \iint T_{y_c} \, dA \qquad M_{y_c} = -\iint T_{z_c} \, x_c \, dA$$

~ ~

CAUTION

The shear components of the linear traction distributions generated by the TLAP Cross Section option do not satisfy the stress free boundary conditions for general cross sectional shapes. Extractions near the area of load application are discouraged.

$$T_{x_c} = \frac{F_{x_c}}{A} - \frac{1}{2} \frac{M_{z_c}}{I_{x_c}} y_c \qquad T_{y_c} = \frac{F_{y_c}}{A} + \frac{1}{2} \frac{M_{z_c}}{I_{y_c}} x_c \qquad T_{z_c} = \frac{F_{z_c}}{A} - \frac{M_{y_c}}{I_{y_c}} x_c + \frac{M_{x_c}}{I_{x_c}} y_c$$

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 $F_{z_c} = \iint T_{z_c} dA \qquad M_{z_c} = \iint T_{y_c} x_c dA - \iint T_{x_c} y_c dA$

TLAP Cross Section Option



GUI Changes for TLAP Cross Section.

StressCheck Input 📧	StressCheck Input
Mesh Section Prop. Thickness Material Load Constr	Mesh Section Prop. Thickness Material Load Constr
Select Any Surface TLAP Traction	Select Face Surface TLAP Traction
Object Method Name Data	Object Method Name Data
· · · · · · · · · · · · · · · · · · ·	│
ID: Set: New set	ID: Set: New set
Scale:	Scale:
Direction: XYZ	Direction: XYZ
System: Global 👻 ि	System: Global 👻 ि
Case ID:	Case ID:
TLAP Option: Cross Section	TLAP Option: Cross Section Vew O
Cocations	Locations
Symbols	Symbols
Labels	Labels
Edit definitions	Edit definitions
Copy load case	Copy load case
	Tolerance: 0.0000e+00
Accent Replace Delete Pume	Accent Beolace Delete Dumo
Edit Deselect	Edit Deselect

The selection needs to satisfy a coplanar condition. If the this condition is not satisfied an error is issued and the record creation is prevented:

ERROR

- Load error found in surfaces/elements = # and #. TLAP Cross Section load applied to faces that are not coplanar. Tolerance may be controlled with parameter COPLANAR TOL (default=0.0001, use a larger value to loosen the tolerance).
- While continuity is not a requirement (multiple selections are allowed) this assignment requires checking a flatness tolerance for the selection (similar as it is done for symmetry or anti-symmetry). If the flatness check does not pass an error is issued and the record is not created:

ERROR

Load error found in surface/element = #. TLAP Cross Section load applied to a surface/face which is not flat.

Tolerance may be controlled with parameter SURFACE TOL (default=0.001 deg.).

Number of points checked on each surface/face controlled with parameter SURFACE MIDPT (default=2). Select face set " FAIL LOAD" to see problem surfaces/faces.

- Same as with other TLAP Traction options multiple load selections are allowed.
- Shown for "Face Surface" but also available for "Face" Object

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ew option









Selections are flat but not coplanar, an error is issued when pressing "Accept"

ERROR

Load error found in elements = # and #, case = LOAD_ID. TLAP Cross Section load applied to faces that are not coplanar. Tolerance may be controlled with parameter _COPLANAR_TOL (default=0.0001, use a larger value to loosen the tolerance).

ERROR

Load error found in surfaces # and #. TLAP Cross Section load applied to surfaces that are not coplanar. Tolerance may be controlled with parameter _COPLANAR_TOL(default = 0.0001, use a larger value to loosen the tolerance). **Cross Section**







ERROR

Load error found in surface = #. TLAP Cross Section load applied to a surface which is not flat. Tolerance may be controlled with parameter _SURFACE_TOL (default = 0.001 deg.). Number of points checked on each surface controlled with parameter _SURFACE_MIDPT(default = 2).Select surface set "_FAIL_LOAD" to see problem surfaces.

ERROR

Load error found in element = #. TLAP Cross Section load applied to a surface which is not flat. Tolerance may be controlled with parameter _SURFACE_TOL (default=0.001 deg.). Number of points checked on each face controlled with parameter _SURFACE_MIDPT (default = 2). Select surface set "_FAIL_LOAD" to see problem surfaces.

Cross Section



TLAP BEARING AND BEARING LOADS CORRECTION

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Definition of Correction loads

Corrective tractions are *added* to the **TLAP bearing** or **Bearing** traction distribution in order to correct the resultants for non-cylindrical holes or suboptimal meshes.

They are *arbitrarily* defined as:

$$T_x = C_1 + C_2 y + C_3 z$$
 $T_y = C_4 + C_5 z$ $T_z = C_6$

In other words, the C_i coefficients are calculated so that the following resultant integrals match the required corrections loads:

$$F_{x} = \iint T_{x} dA \qquad F_{y} = \iint T_{y} dA \qquad F_{z} = \iint T_{z} dA$$
$$M_{x} = \iint (-T_{y}z + T_{z}y) dA \qquad M_{y} = \iint (T_{x}z - T_{z}x) dA \qquad M_{z} = \iint (-T_{x}y + T_{y}x) dA$$



$M_{y} = \iint (C_{1}z + C_{2}yz + C_{3}z^{2} - C_{6}x)dA = C_{2}I_{yz} + C_{3}I_{zz}$ $M_{z} = \iint (-C_{1}y - C_{2}y^{2} - C_{3}yz + C_{4}x + C_{5}zx)dA = -C_{2}I_{yy} - C_{3}I_{yz} + C_{5}I_{zx}$

Calculation of correction loads

The expanded resultant correction integrals are:

$$F_{x} = \iint (C_{1} + C_{2}y + C_{3}z)dA = C_{1}A \Longrightarrow C_{1} = \frac{F_{x}}{A}$$

$$F_{y} = \iint (C_{4} + C_{5}z)dA = C_{4}A \Longrightarrow C_{4} = \frac{F_{y}}{A}$$

$$F_{z} = \iint C_{6}dA = C_{6}A \Longrightarrow C_{6} = \frac{F_{z}}{A}$$

$$M_{x} = \iint (-C_{4}z - C_{5}z^{2} + C_{6}y)dA = -C_{5}I_{zz} \Longrightarrow C_{5} = -\frac{M_{x}}{I_{zz}}$$

$$M_{y} = \iint (C_{1}z + C_{2}yz + C_{3}z^{2} - C_{6}x)dA = C_{2}I_{yz} + C_{3}I_{zz}$$

$$T_z$$
 T_y T_x y x

STRESSCHE

(x, y, z) is centroidal

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(x, y, z) is centroidal

RESS

Calculation of correction loads

Calculation of correction loads

The corrective tractions are therefore given as:

$$T_{x} = \frac{F_{x}}{A} - \frac{M_{y}I_{yz} + M_{z}I_{zz} + M_{x}I_{zx}}{(I_{yy}I_{zz} - I_{yz}^{2})}y + \frac{M_{y}I_{yy} + M_{z}I_{yz} + \frac{M_{x}}{I_{zz}}I_{zx}I_{yz}}{(I_{yy}I_{zz} - I_{yz}^{2})}z$$

$$T_{y} = \frac{F_{y}}{A} - \frac{M_{x}}{I_{zz}}z$$

$$T_z = \frac{F_z}{A}$$

Bearing loads are defined as an approximation used to represent the pressure distribution caused by a lightly loose fit pin in contact with a perfect cylindrical hole. Deviations from that case (pin interference or hole geometry) will result on entirely different pressure distributions to that of the bearing formula.



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Changes on the GUI: Bearing Load





StressCheck Input

Material Load Constraint Solution ID p-Discretization	Material Load Constraint Solution ID p-Discretization	ion I i
Select Any Surface	Select Face Surface TLAP Bearing Select Face TLAP Bearing TLAP Bearing	For files prior 10.5 anv
Object Method Name Data	Object Method Name Data	existing TLAP Bearing
ID: Set: New set	D: Set: New set	record will be read with
Scale:	Scale:	the toggle off (no
Direction: Vector	Direction: Vector	correction applied)
System: Create Auto	System: Global V & System: Global V &	
Case ID:	ase ID:	
	Autocorrect Adjust th	ne bearing distribution to correct the resultant load
TLAP Option: Default	tion: Default	t t
	Locations Locations	Tooltip
Symbols	Symbols Symbols	
Labels	Labels	
Edit definitions	Edit definitions Edit definitions	
Copy load case	Copy load case Copy load case	
	Tolerance: 0.0000e+00	
Accept Replace Delete Purge	Accept Replace Delete Purge Accept Replace Delete P	ırge
Edit Deselect	Edit Deselect Edit Deselect	

StressCheck Input

Changes on the GUI: TLAP Bearing

StressCheck Input



Additional changes



Error and Warning messages for TLAP bearing:

 When using Autocorrect, previous circularity and tapper error have been replaced with errors related to invalid selection and warning messages for circularity and correction tolerances:

ERROR

The selected surface type is invalid for TLAP bearing loads (only cylindrical type surfaces can be used). The record has not been created.

WARNING

Circularity tolerance exceeded for TLAP bearing load ID: LoadID (SET#):

The difference in max. and min. radius (#.######) is ##.####% different than the estimated avg. radius (#.#######). This may indicate that element faces do not resemble a cylindrical hole, or that the chosen system is not aligned with the hole centerline. If this is unexpected, check your selection for unintended surfaces or faces. Define a value for parameter _bearing_tol to redefine the tolerance check.

WARNING

The total resultant force and/or moment for TLAP bearing load ID: LoadID (SET#) are being corrected by #% with respect to the local system. This may occur if the element faces do not resemble a cylindrical hole. If this is unexpected, check your selection for unintended surfaces or faces. Alternatively you can define a value for parameter _bearing_correction_tol to redefine the tolerance check (currently 0.05).

Input resultants (local dir.) are Fx: #.##e+##, Fy: #.##e+##, Fz: #.##e+##, Mx: #.##e+##, My: #.##e+##, Mz: #.##e+## Computed resultants (local dir.) are Fx: #.##e+##, Fy: #.##e+##, Fz: #.##e+##, Mx: #.##e+##, My: #.##e+##, Mz: #.##e+## Correction values (local dir.) are Fx: #.##e+##, Fy: #.##e+##, Fz: #.##e+##, Mx: #.##e+##, My: #.##e+##, Mz: #.##e+##

Additional changes



• Error and Warning messages for **Bearing** loads:

 When using Autocorrect, previous circularity and tapper error have been replaced with errors related to invalid selection and warning messages for system selection, circularity and correction tolerances:

ERROR

The selected surface type is invalid for Bearing loads (only cylindrical type surfaces can be used). The record has not been created.

WARNING

The chosen system for bearing load ID: Load (SET#) is significantly offset from the hole centroidal axis. Please check your system selection to ensure it is aligned with the hole.

WARNING

Circularity tolerance exceeded for bearing load ID: LoadID (SET#):

The difference in max. and min. radius (#.######) is ##.####% different than the estimated avg. radius (#.#######). This may indicate that element faces do not resemble a cylindrical hole, or that the chosen system is not aligned with the hole centerline. If this is unexpected, check your selection for unintended surfaces or faces. Define a value for parameter _bearing_tol to redefine the tolerance check.

WARNING

The total resultant force and/or moment for bearing load ID: LoadID (SET#) are being corrected by #% with respect to the local system. This may occur if the element faces do not resemble a cylindrical hole. If this is unexpected, check your selection for unintended surfaces or faces. Alternatively you can define a value for parameter _bearing_correction_tol to redefine the tolerance check (currently 0.05).

Input resultants (local dir.) are Fx: #.##e+##, Fy: #.##e+##, Fz: #.##e+##, Mx: #.##e+##, My: #.##e+##, Mz: #.##e+## Computed resultants (local dir.) are Fx: #.##e+##, Fy: #.##e+##, Fz: #.##e+##, Mx: #.##e+##, My: #.##e+##, Mz: #.##e+## Correction values (local dir.) are Fx: #.##e+##, Fy: #.##e+##, Fz: #.##e+##, Mx: #.##e+##, My: #.##e+##, Mz: #.##e+##

Acceptable deviations from cylindrical holes

Acceptable variations include:

- 1. General case: Conical cylinder with elliptical tapered ends.
- 2. Embedded cracks
- 3. Additional (any shape) holes
- 4. Truncated*
- 5. Faceted (element faces not mapped directly on the

cylindrical surface)

Note that the Bearing load correction acts correcting the resultants based on input. Therefore if the bearing load direction is so that part or all of the bearing formula is not acting on any elements the resultant will still be corrected so that it is the same as the input.





STRESS

New Any Body option for Assignment

Any Body option for Assignment: Material Assign – Load – p-Discretization tabs



Note: "Mesh Region" and "Any Body" methods are

- complementary in the following sense:
- Elements created inside the body but not associated to the body will not be recognized by the option "Any Body" but will be by the option "Mesh Region".
- Elements associated to the body that are not fully contained in the body will not be recognized by the option "Mesh Region" but will be recognized by the option "Any Body".

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Object Material ID System Al/Set Object Method Name D(Themal ID: • Set: New set Scale: • System: Global • X: 0.0 Z: 0.0 Z: 0.0 Accept Replace Delete Parage Ect Deselect Deselect • Deselect	Select Any Body Select New option	Select Any Body Body Force	Select
ID: Set: Scale: System ID: Loopt Replace Purge Replace Purge Replace Detete Purge Replace Detete Purge Edit Deselect	Object Material ID System All/Set	Object Method Name D{Thermal	p-Discr. Space p All/Set Type
ID: Set: Scale: System Global Color Steel Drection: X/Z System: Global No Z: 0.0 Define Perfore Define Purge Cotor Pring Dester Purge Cit Dester Purge Dester Purge Dester Purge			↓
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Fitting Deselect	Accept Replace Delete Purge	Accept Replace Delete Purge	Accept Replace Delete Purge
	Fitting Deselect	Edit Deselect	Deselect





Plastic strains can be computed from the total strain and mechanical strain components.

 $\varepsilon_x^p = \varepsilon_x - \frac{1}{E} (\sigma_x - \nu \sigma_y - \nu \sigma_z) - \alpha T_\Delta$ Total Strain Elastic strain Plastic strain $\varepsilon_{ij} = \varepsilon_{ij}^{e} + \varepsilon_{ij}^{p} + \alpha T_{\Delta} \delta_{ij}$ Thermal strain $\varepsilon_{y}^{p} = \varepsilon_{y} - \frac{1}{E} \left(-\nu \sigma_{x} + \sigma_{y} - \nu \sigma_{z} \right) - \alpha T_{\Delta}$ $\varepsilon_{z}^{p} = \varepsilon_{z} - \frac{1}{F} \left(-\nu \sigma_{x} - \nu \sigma_{y} + \sigma_{z} \right) - \alpha T_{\Delta}$ $\gamma_{xy}^{p} = 2\varepsilon_{xy}^{p} = \gamma_{xy} - \frac{2(1+\nu)}{F}\tau_{xy} = \gamma_{xy} - \frac{\tau_{xy}}{F}$ $\varepsilon_{ii}^p = \varepsilon_{ii} - \varepsilon_{ii}^e - \alpha T_\Delta \delta_{ii}$ $\begin{vmatrix} \gamma_{yz}^{p} = 2\varepsilon_{yz}^{p} = \gamma_{yz} - \frac{\tau_{yz}}{G} \\ \gamma_{zx}^{p} = 2\varepsilon_{zx}^{p} = \gamma_{zx} - \frac{\tau_{zx}}{G} \end{vmatrix}$ $\varepsilon_{ij}^{p} = \varepsilon_{ij} - \frac{1+\nu}{F}\sigma_{ij} + \frac{\nu}{F}\sigma_{kk}\delta_{ij} - \alpha T_{\Delta}\delta_{ij} \bigg]$



Principal, and Equivalent plastic strains:

$$\sigma_{eq} \stackrel{\text{def}}{=} \sqrt{\frac{3}{2}} S_{ij} S_{ij} = \sqrt{\frac{3}{2}} \left(\sigma_{ij} - \frac{1}{3} \sigma_{kk} \delta_{ij} \right) \left(\sigma_{ij} - \frac{1}{3} \sigma_{kk} \delta_{ij} \right) = \frac{E}{(1+\nu)} \sqrt{\frac{3}{2}} \left(\varepsilon_{ij} - \frac{1}{3} \varepsilon_{kk} \delta_{ij} \right) \left(\varepsilon_{ij} - \frac{1}{3} \varepsilon_{kk} \delta_{ij} \right)$$

$$\sigma_{eq} = \frac{E}{(1+\nu)} \sqrt{\frac{1}{2}} \left[(\varepsilon_1 - \varepsilon_2)^2 + (\varepsilon_2 - \varepsilon_3)^2 + (\varepsilon_3 - \varepsilon_1)^2 \right]} \qquad \varepsilon_{eq} \stackrel{=}{\underset{\sigma_{eq} := E}{=}} \frac{1}{\varepsilon_{eq}} \frac{1}{(1+\nu)} \sqrt{\frac{1}{2}} \left[(\varepsilon_1 - \varepsilon_2)^2 + (\varepsilon_2 - \varepsilon_3)^2 + (\varepsilon_3 - \varepsilon_1)^2 \right]}$$

For plastic strains $\nu = 0.5$

Principal plastic strains are computed as:

$$\left[\begin{array}{c} \\ \\ \\ \\ \end{array} \right] \varepsilon_{eq}^{p} = \sqrt{\frac{2}{9} \left[\left(\varepsilon_{1}^{p} - \varepsilon_{2}^{p} \right)^{2} + \left(\varepsilon_{2}^{p} - \varepsilon_{3}^{p} \right)^{2} + \left(\varepsilon_{3}^{p} - \varepsilon_{1}^{p} \right)^{2} \right]}$$

$$\left| \varepsilon_{ij}^{p} - \varepsilon^{p} \delta_{ij} \right| = 0$$
$$\varepsilon_{1}^{p} \ge \varepsilon_{2}^{p} \ge \varepsilon_{3}^{p}$$



 The new extraction functions are available for the Plot, Min/Max and Points tabs in the Results StressCheck dialog.





Tvz

LOG IMPROVEMENTS FOR INCREMENTAL THEORY OF PLASTICITY (ITP) SOLUTIONS

TM

Log Improvements for ITP Solutions



EXECUTION SETUP SETTINGS:

Title = Plate with offset hole Reference = 2D Theory = Elasticity Solution ID = NSOL Startup = Initialize Convergence = Upward Iteration = Automatic Run type = Nonlin-Mat Run Limit = 1 Elastic-Plastic Analysis (Incremental Theory of Plasticity) Nonlinear ID: NSOL Linear ID: SOL, Linear run: 8 Nonlinear convergence criteria = Displacement Tolerance (%) = 5.000e-03, Iteration Limit: 10 Number of Events: 4

Coalesced the information shared by all Events/Steps and included selected theory

Log Improvements for ITP Solutions



Event: 1 - Cold-Working • Event name and number, as well as the Step: 1 of 2 Solution ID: NSOL 8 1 1 solution name for each step are now logged. Boundary Condition Parameters: Delta = 0.0115Parameters defined as B. Cond. are added $Emf = 3e \pm 07$ $T_X = 0$ to the log together with their corresponding Pf = 0Convergence information: value for a given Event/Step. Iteration 1: Largest error = 100.000% at element 2, total unconverged elements = 38 Iteration 2: Largest error = 27.547% at element 38, total unconverged elements = 38 Iteration 3: Largest error = 5.575% at element 5, total unconverged elements = 38 Convergence information for each load Iteration 4: Largest error = 1.238% at element 5, total unconverged elements = 38 Iteration 5: Largest error = 0.072% at element 5, total unconverged elements = 38 step is contained within the Event Iteration 6: Largest error = 0.000% at element 5, total unconverged elements = 0 Step solution time = 16 seconds. Step: 2 of 2 NSOL 8 1 2 Solution ID: Boundary Condition Parameters: Delta = -0.001Emf = 1000Tx = 0Pf = 0Convergence information: Iteration 1: Largest error = 77.675% at element 38, total unconverged elements = 38 Iteration 2: Largest error = 0.540% at element 41, total unconverged elements = 38 Iteration 3: Largest error = 0.003% at element 8, total unconverged elements = 0 Step solution time = 8 seconds.





Name sorting for ITP solutions



Re	sult	s StressO	he	ck					
	Error	Plot		Min/Max	Points	Res	ultant	4	۲
	Sele	ct	•	All Elemer	nts 🔻	Select	tion	•	
ľ	Solu	tion		Ru	n Typ	e	DOF		
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	CW	511		.1	.NLMat		1874		11
	CW	512		, 2	, NLMat		1874		
	CW	521		, 3	, NLMat		1874		
	CW	5_3_1		, 4	, NLMat	,	1874		
	CW	5_3_2		, 5	, NLMat	,	1874		
	CW	5_3_3		,6	, NLMat		1874		
	CW_	5_3_4		,7	, NLMat		1874		
lì	CM_	5_3_5		, 8	,NLMat		1874	=	
	CW_	5_3_6		, 9	,NLMat		1874	-	
	CW_	5_3_7		,10	,NLMat		1874		
	CW_	5_3_8		,11	,NLMat		1874		
	CW_	5_3_9		, 12	,NLMat		1874		
	CM_	5_3_10)	,13	, NLMat		1874		
	CM_	5_3_11	1	,14	, NLMat		1874		
Į,	CM	5_3_12	2	,15	,NLMat		1874	-	
	CM_	5_3_13	3	,16	,NLMat		1874		
	CM	5_3_14	L .	,17	,NLMat		1874		
	CM	5_3_15	5	,18	,NLMat		1874		
	CM	5_3_16	5	,19	,NLMat		1874		
	CM	5_3_17	7	,20	,NLMat		1874		
	CM	5_3_18	3	,21	,NLMat		1874		
	CM ⁻	5_3_19	•	, 22	,NLMat		1874		
	CM ⁻	5_3_20)	,23	,NLMat		1874		
	CM	5_3_21	-	,24	,NLMat		1874		
	CM-	5_3_22		,25	,NLMat		1874		
	CM-	5_3_23	3	,26	,NLMat		1874		
L	CM	5_3_24		,27	, NLMat		1874		
	CM_	5_3_25	5	,28	,NLMat		1874		
	CM	5_3_26	2	,29	, NLMat		1874		
	CW	5 3 27		, 30	,NLMat		1874	T	

IPT solutions are now sorted *sequentially* based on linear solution run, Event and Step number respectively.



Face/Face Surface element blank

Use Face or Face Surface selection to blank elements:



STRESSCHECK



Curves resolution can now be controlled



FILE BUILD NUMBER IS NOW RECORDED IN THE PROJECT LOG

TM



File Build number is now recorded in the Project Log

Previous project log entries from the original file

Ø Project Log				
Dec 12 2018 10:05:41AM New	v Project			
Dec 14 2018 05:12:23PM Sav	ved project C:\Work\Test.scp			New log entry. When opening an
Feb 26 2019 01:45:41PM Ope	ened file C:\Work\Test.scw (V	10.4.50606)	•	existing file, the version and build number from which it was last saved are displayed.



LONG SOLUTION NAMES ARE NOW WRAPPED ON THE PLOT LEGEND

TM

Long solution names





AUTOMATIC AND MANUAL SELECTION OF GRAPHIC DRIVERS

TM





Options 🛛 🕅	
Path to Scratch Directory:	
D:\Temp Browse	
Startup: Input 👻	
Units: in/lbf/sec/F 🔻	
Graphics: Auto	
Line Thickness: 1	
Edge Resolution: 2	
Display Format: %11.4e	
Courier New, 10 pt. Display Font	
Lucida Console,9 pt. Legend Font	
Show warning messages	
V Trace boundaries	
Perspective	
Show Project Log at startup	
Default OK Cancel Apply	

- By default, StressCheck[®] automatically selects the most appropriate graphics driver based on the current runtime environment.
- In case needed or desired by the user an option has been added in the Options dialog to choose between driver preferences: Automatic, DirectX 11, DirectX 9, OpenGL 2, and OpenGL.
- The Check button displays a message indicating which driver is currently in use, the recommended selection (Auto), and the stored preference





TM

QUESTIONS OR COMMENTS?

Contact support@esrd.com